
Hydrological Analysis and Peak Runoff Determination in Basaka River Sub-Watershed, Abbay Basin, Ethiopia Using Gumbel's and SCS Methods Respectively

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To cite this article:

Gemechu Mosisa, Kuma Abebe, Yadesa Wakena. Hydrological Analysis and Peak Runoff Determination in Basaka River Sub-Watershed, Abbay Basin, Ethiopia Using Gumbel's and SCS Methods Respectively. *Journal of Water Resources and Ocean Science*.

Vol. 12, No. 2, 2023, pp. 23-30. doi: 10.11648/j.wros.20231202.11

Received: October 9, 2023; **Accepted:** October 25, 2023; **Published:** November 11, 2023

Abstract: Peak runoff determination is one of the most important studies for the design of hydraulic structures which is used for different purposes like irrigation, water supplies, hydropower, and bridge structure. The amount of runoff produced and rainfall received determine the development of water resources in any region. The purpose of hydrologic design is to estimate the maximum, average, or minimum flood that the structure is expected to handle. Hydrological analysis has been conducted based on 33 years of maximum daily rainfall data. An important step in the analysis of rainfall occurrence is to choose an appropriate distribution to represent the depth of rainfall to study rainfall. Nekemte meteorological station was used for maximum rainfall estimation by gumbles distribution method of 50 & 100 years return period which is 132 & 142mm; while for generation of peak runoff by using soil conservation service (SCS) method which is 238 & 263m³/s respectively for Basaka sub-watershed. Conversely, the SCS method is recommended to estimate the ordinate required for the development of peak runoff hydrograph in the river sub-watershed because it utilized additional morphometric parameters such as watershed slope and the curve number (CN) which is a function of the properties of the soil and vegetation cover of the watershed. Basaka sub-watershed delineation analysis was done by GIS 10.8 and it covers a drainage area of about 58km².

Keywords: SCS, Gumbel, Basaka Sub-Watershed, Peak Runoff, Maximum Rainfall

1. Introduction

Hydrology is broadly defined as the geosciences that describe and predict the occurrence, circulation, and distribution of water in the earth and its atmosphere [1]. The study of hydrology helps us to know the maximum probable flood that may occur at a given site and its frequency; this is required for the safe design of drains and culverts, dams and reservoirs, channels, and other flood control structures [2]. Another purpose is to know the water yield from a basin its occurrence, quantity, and frequency; this is necessary for the design of dams, municipal water supply, water power, and river navigation. And also to determine the maximum intensity of the storm and its frequency for the design of a drainage project in the area [3]. Hydrologic design is important for the safety, economy, and proper functioning of hydraulic structures. The purpose of hydrologic design is to estimate the

maximum, average, or minimum flood that the structure is expected to handle. This estimate has to be made quite accurately in order for the project can function properly [4]. For the design and analysis of structures to be constructed on the river, estimation of flood magnitude is an important task. This can be done using different techniques depending on the data available. For this particular case, there is no river flow data, and hence the flood estimation is done using the rainfall data and applying the SCS Curve Method [5, 6]. Extreme values of rainfall are of prime interest as inputs to simulation models used to estimate design floods. The design flood is then a basis for the designing of hydraulic structures, and drainage systems such as diversion weirs, dams, and cross-drainage structures [7]. The aim of this paper is to estimate the peak runoff for the Basaka sub-watershed. Most importantly the following evaluations will be carried out such as time series data analysis of the daily rainfall, catchment

features pertinent to the analysis and simulation of hydrological data, rainfall (length of records, daily distribution and its intensity, average values) data collection and analysis, and estimation of incoming floods to the river sub-watershed.

2. Materials and Methods

2.1. Location and Description of the Study Area

The Basaka River sub-watershed is located in the Abbay basin which is found in the western part of Ethiopia. The area has high potential water and land suitable for irrigation

development. The project area is located about 20km from Nekemte Town. It covers a drainage area of about 58 km². Basaka sub-watershed has latitude and longitude of 8°59'30"N to 9°6'30"N and 36°30'00"E to 36°37'30"E an elevation of 2075 meters and receives an annual average rainfall of 2059 mm as shown in Figure 1 blow. The annual rainfall data for 33 years (1990-2022) were collected from the Ethiopian Meteorological Institute (EMI) for Nekemte station; the extreme rainfall events for the years commencing from 1990-2022 were observed.

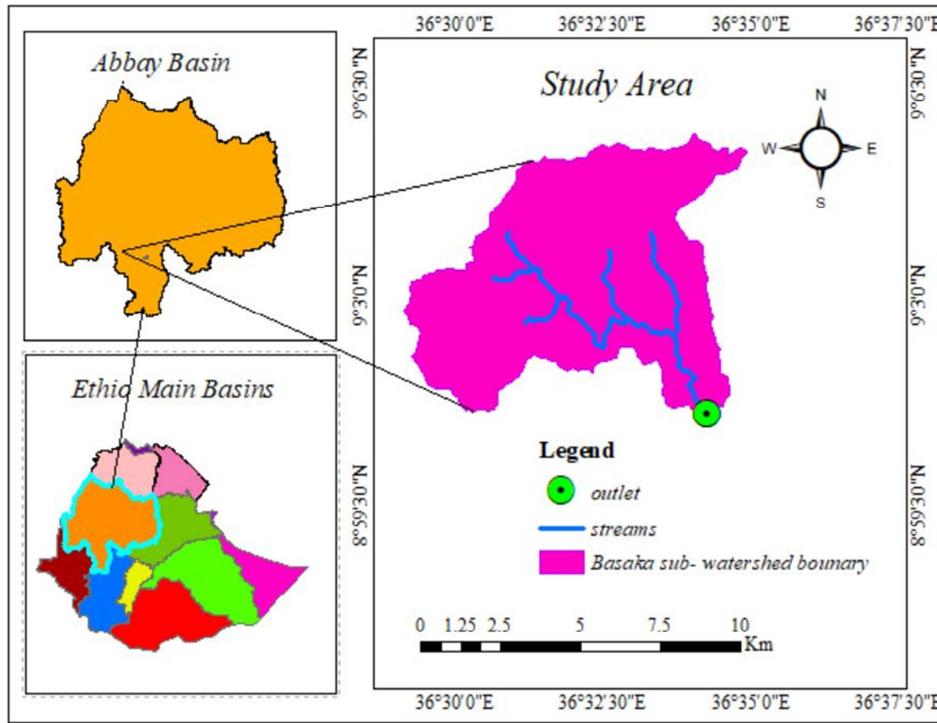


Figure 1. Location map of the study.

2.2. Methods

Table 1. Methods and soft wares used during this study.

S.No	Types of used methods and software	Function
1	SCS method	Was used to estimate the peak runoff of the Basaka River sub-watershed
2	Gumbel method	Was used to estimate the maximum rainfall of the Basaka River sub-watershed
3	ArcGIS10.8	To delineate the Sub-watershed of the study area, to know LULC, hydrologic soil group, and to get the longest flow path
4	30*30 DEM	Was used as input data for ArcGIS software for catchment delineation and estimation of catchment characteristics.
5	Excel software	To use the estimation of mathematical equations

2.3. Digital Elevation Model of the Study Area

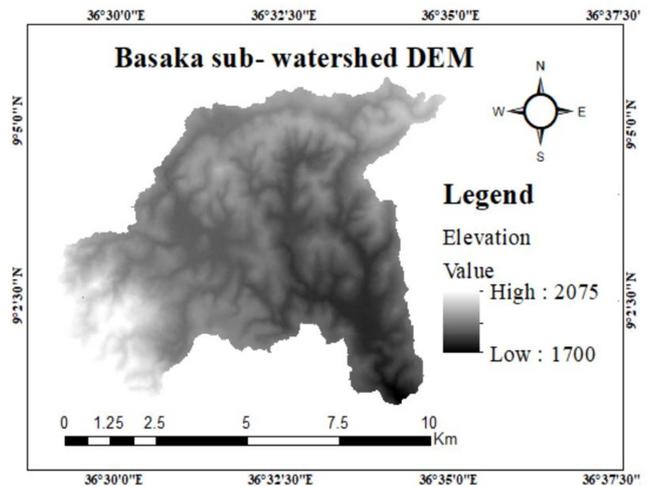


Figure 2. Digital elevation model of the Basaka sub-watershed.

The digital elevation model is one of the crucial inputs for the Arc Hydro tool in GIS to calculate the flow accumulation, stream networks, slope, stream length, and width of the channel and to delineate drainage networks of the watershed and sub-watersheds. Also, DEM is the digital representation of the land surface elevation concerning to any reference data and is frequently used for any type of work that refers to the digital representation of a topographic surface. A 30m by 30m resolution Advanced Space Borne Thermal Emission and Reflection Radiometer (ASTER) Global Digital Elevation Model was obtained from the Ministry of Water, Irrigation & Energy (MOWIE).

2.4. Land Use Land Covers Classification of Basaka Sub-Watershed

Land use land cover is also another factor that is used to evaluate the land for irrigation suitability based on the determination of peak runoff which is used for the design of hydraulic structures like diversion weir. The 2022, 30m resolution land use land cover map of the watershed was accessed from ArcGIS Living Atlas of the World. Land use land cover influences the cost of irrigation practices to prepare the land for agriculture. It was taken as one input for the evaluation of land qualities for irrigation for the study area. Vegetation and rock are the most common cover types that require removal for successful irrigation. Rocks may also be a factor in the construction of farm distribution and drainage systems and land grading operations. The type of land use land cover in the study area included grassland, bare land, cultivated land, forest land, built area, and water bodies as shown in Figure 3 below.

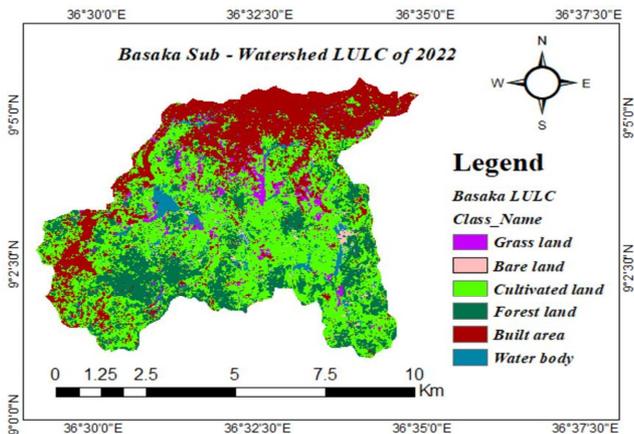


Figure 3. The LULC map of Basaka sub-watershed in 2022.

2.5. Soil Data Analysis

Soil data were obtained from the Ethiopian Ministry of Water, Irrigation and Energy (MOWIE), and they were pre-processed to follow the Food and Agricultural Organization (FAO) guidelines as stated in [8]. Two soil types can be recognized in the Basaka sub-watershed those are Humic Cambisols, and Eutric Nitosols as shown in Figure 4.

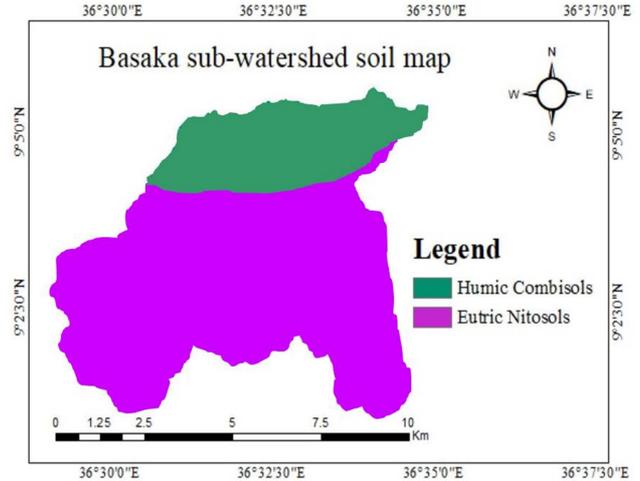


Figure 4. Soil map of the Basaka sub-watershed.

2.6. Analysis of Rainfall by Gumbel Method

In the analysis of rainfall frequency, the probability of occurrence of a particular extreme rainfall (daily maximum rainfall) is important. This data can be found by analyzing the frequency of point rainfall depth. Then the probability of occurrence of point rainfall (daily maximum rainfall) is estimated for a recurrence interval of 50 years, for the diversion weir [5, 6, 8-13]. The prediction of peak flows from rainfall over catchments involves the estimation of daily maximum rainfall for a given return period and conversion of the daily maximum rainfall to runoff hydrograph at the desired location. The Gumbel method is the most broadly used probability distribution function for extreme value in hydrological and metrological studies for the prediction of peak floods from maximum rainfall [4, 6, 9, 13-17].

$$X_T = \bar{X} + K * \sigma_{n-1} \tag{1}$$

Where

X_T = Annual peak rainfall of T return period (mm)

\bar{X} = Mean rainfall data (mm)

σ_n = is the standard deviation of the sample size of N

$$\sigma_{R-1} = \sqrt{\frac{\sum(X-\bar{X})^2}{N-1}} \tag{2}$$

K = Frequency factor expressed as,

$$K_T = \frac{YT - Y_n}{S_n} \tag{3}$$

YT is a reduced variant for a given T, given by

$$YT = -\ln \left(\ln \left(\frac{T}{T-1} \right) \right) \tag{4}$$

Y_n & S_n = Reduced mean and standard deviation respectively, a function of sample size N and obtained from standard table [16] cited by [6].

2.7. Area Reduction Factor

The rainfall obtained from the rain gauge station is a point

rainfall. This point rainfall should be transferred to the catchment area rainfall by multiplying it by the area reduction factor (ARF) as obtained in the following formula [17]:

$$\text{Areal reduction Factor (ARF)} = 1 - 0.044A^{0.275} \quad (5)$$

2.8. Peak runoff Generation Using the SCS Method

According to Subramanya [18], for 50 to 100 years of return periods, however, one should fit a theoretical distribution to the flood data. And also requires meteorological data for a minimum of 30 years for meaningful predictions [19]. The peak runoff for incremental rainfall was calculated using the technique developed by the US Soil Conservation Service which is a widely used method [20].

$$Q = \frac{(P-I_a)^2}{(P-I_a+S)} \quad (6)$$

Where: Q = accumulated direct runoff, mm

P = accumulated rainfall (potential maximum runoff), mm

$$I_a = 0.2S \quad (7)$$

I_a - is initial abstraction including surface storage, interception, and infiltration prior to Runoff, mm

$$Q = \frac{(P-0.2S)^2}{(P+0.8S)} \quad (8)$$

$$S = \frac{25400}{CN} - 254 \quad (9)$$

S = potential maximum retention, mm

2.9. Time of Concentration (TC)

It means the time required for runoff to travel from the hydraulically most distant point in the watershed to the outlet [21]. TC is generally applied only to surface runoff and varies depending on the slope and character of the watershed and the flow path. It has been calculated by taking the stream length of the longest streamline and slope. Kirpich formula is cited by [6, 8, 19, 21, 22], and adopted for computation.

$$T_c = \frac{1}{3000} * \left(\frac{L}{\sqrt{S}}\right)^{0.77} \quad (10)$$

Where: L= length (m), S = slope (m/m)

$$\text{Duration of excess rainfall (hr), } D = \frac{T_c}{6} \quad (11)$$

3.2. Land Use Land Covers Classification Analyzed and Result

Table 2. Analyzed of 2022 LULC of the Basaka sub-watershed.

S.NO	Conditions	Year (2022)		HSG	CN	CN*A
		Area in km ²	Area %			
1	Built up area	5.45	9.4	C	90	490.5
2	Bare land	1.5	2.6	B	86	129
3	Cultivated Land	30	51.7	B	78	2340
4	Grass Land	8.75	15.1	C	74	647.5
5	Forest Land	10.25	17.7	C	73	748.3
6	Water Body	2.05	3.5	B	100	205
Total		58	100.0			4560.3

$$\text{Time to peak, } T_p = 0.5D+0.6*T_c \quad (12)$$

$$\text{Time of base of hydrograph } T_b = 2.67*T_p \quad (13)$$

$$\text{Lag time, } T_l = 0.6 * T_c \quad (14)$$

$$\text{Peak runoff determination, } Q_p = \frac{0.21*A}{T_p} \quad (15)$$

Computation curve number (CN) from ArcGIS software result

$$CNII = \frac{(\sum CN * A)}{\sum A} \quad (16)$$

$$AMCIII = \frac{23*AMCII}{10+0.13AMCII} \quad (17)$$

3. Results & Discussion

3.1. Result of Rainfall Analysis Using Gumbel's Method

3.1.1. Result of Rainfall Analysis for 50 Years Return Period

$$X_T = \bar{X} + K * \sigma_{n-1}$$

$$\bar{X} = 79\text{mm}, \sigma_{n-1} = 25\text{mm}, K=2.9, Y_T = 3.902, Y_n = 0.5485, S_n = 1.1607$$

$$X_{50} = 79 + 2.9*25 = 152\text{mm}$$

Hence, the design of point rainfall =152mm.

Where A is catchment area (km²) = 58km², by using peak point rainfall from Gumbel's distribution method areal rainfall can be calculated as, $A_{RF} = 0.866$

$$\text{Areal design Rainfall (ADR)} = A_{RF} * \text{peak point rainfall} = 0.866*152\text{mm} = 132\text{mm}$$

3.1.2 Result of Rainfall Analysis for 100 Years Return Period

$$K=2.9, Y_T = 3.902, Y_n = 0.5600, S_n = 1.2065$$

$$X_{100} = 79 + 3.4*25 = 164\text{mm}$$

Hence, the design of point rainfall =164mm.

$$\text{Areal design Rainfall (ADR)} = A_{RF} * \text{peak point rainfall} = 0.866*164\text{mm} = 142\text{mm}$$

3.3. Soil Data Analyzed and Result

Table 3. Analyzed soil types of Basaka sub-watershed.

S.NO	Soil group name	SWAT-Code	HSG	Area Km2	Area %
1	Humic Cambisols	Bh12-3c-31	C	15.25	26.3
2	Eutric Nitosols	Ne13-3b-158	B	42.75	73.7
Total			58		100

$$CN_{II} = \frac{\sum CN * Area}{\sum Area} = \frac{4508.15}{58} = 78.6, \quad CN_{III} = \frac{23 * CN_{II}}{10 + 0.13 * CN_{II}} = 89.4$$

3.4. Generation of Peak Runoff Using the SCS Method

Table 4. Determination of peak Runoff by Soil Conservation Service (SCS) method.

A summary of peak runoff by using SCS of Basaka River sub-watershed in 50 years return period				
No.	Designation and Formula	Symbol	Unit	Value
1	Area of catchment (this can be determined from 1:50,000 scale topographical maps or aerial photographs)	A	Km ²	58
2	Length of main water course from watershed divide to proposed diversion or storage site (Topographic maps)	L	M	20000
3	Elevation of water shed divide opposite to the head of the main watercourse (Topographic maps)	H1	M	2075
4	Elevation of stream bed at proposed or storage site (Topographic maps)	H2	M	1700
5	The slope of the main watercourse, S	S	m/m	0.02
6	Time of Concentration	TC	Hr	3.1
7	Rainfall excess duration	D	Hr	0.5
8	Time to peak	Tp	Hr	2.1
9	Time of base of the hydrograph	Tb	Hr	5.5
10	Lag time	Tl	Hr	1.86
11	Peak rate of discharge created by 1mm rainfall on the whole of the catchment	Qp	m ³ /s/m	5.8

Table 5. Determination of rainfall profile and areal rainfall.

12	13	14	15	16	17	18	19
Duration	Daily point rainfall of return period 50-year	Rainfall Profile	Rainfall Profile	Areal to point rainfall	Areal rainfall	Incremental rainfall	Descending order
hr	mm	%	mm	%	mm	mm	No.
0- 0.5	132	30	39.6	59.7	23.6	23.6	1
0.5- 1		45	59.4	69.7	41.4	17.8	2
1-1.5		54	71.3	73.4	52.3	10.9	3
1.5- 2		59	77.9	77.0	60.0	7.6	4
2-2.5		65	85.8	79.0	67.8	7.8	5
2.5 -3		67	88.4	81.0	71.6	3.8	6

Table 6. Determination of the time of incremental hydrograph.

20	21	22	23	24	25
Rearranged order	Rearranged incremental rainfall	Cumulative rainfall	Time of incremental hydrograph		
			Time of beginning	Time to peak	Time to end
No	mm	mm	hr	hr	hr
6	3.8	3.8	0	2.1	5.5
4	7.6	11.4	0.5	2.6	6.0
3	10.9	22.3	1	3.1	6.5
1	23.6	45.9	1.5	3.6	7.0
2	17.8	63.7	2	4.1	7.5
5	7.8	71.5	2.5	4.6	8.0

Table 7. Determination of direct runoff.

No	Designation and Formula	Symbol	Unit	Magnitude
26	Find the maximum potential difference between rainfall (p) and direct runoff (Q), which is given by the following formula: CN = 89.4	S	mm	30
27	Substitute the value of "S" in the following formula, giving the relation between direct runoff (Q) and rainfall (P)	Q	mm	
28	Using $Q = \frac{(P-0.2S)^2}{(P+0.8S)}$, it is possible to define the direct runoff Q,(mm)	Col=22	Col=34	
		mm	mm	
		3.8	0.2	
		11.4	0.8	
		22.3	5.7	
		45.9	22.8	

No	Designation and Formula	Symbol	Unit	Magnitude
		63.7	38.0	
		71.5	44.9	

Table 8. Determination of Peak runoff increment based on incremental runoff.

29	30	31	32	33			
Duration	Cumulative runoff	Incremental Runoff	Peak runoff for increment	Time of beginning	Time to peak	Time to end	
hr	mm	mm	m ³ /s	hr	hr	Hr	
0- 0.5	0.2	0.2	1.2	0	2.1	5.5	
0.5- 1	0.8	0.6	3.5	0.5	2.6	6.0	
1-1.5	5.7	4.9	28.4	1	3.1	6.5	
1.5- 2	22.8	17.1	99.2	1.5	3.6	7.0	
2-2.5	38.0	15.2	88.2	2	4.1	7.5	
2.5 -3	44.9	6.9	40.0	2.5	4.6	8.0	

Table 9. Determination of Unit Hydrograph.

Time(hr)	Unit Hydrograph					
	1	2	3	4	5	6
To	0	0.5	1	1.5	2	2.5
Qo	0	0	0	0	0	0
Tp	2.1	2.6	3.1	3.6	4.1	4.6
Qp	1.2	3.5	28.4	99.2	88.2	40.0
Tb	5.5	6	6.5	7	7.5	8
Qo'	0	0	0	0	0	0

Table 10. Determination of Composite Hydrograph.

Time(hr)	Composite Hydrograph(m ³ /s)							Remark
	Q1	Q2	Q3	Q4	Q5	Q6	QT	
0	0						0	
0.5	0.3	0					0	
1	0.6	0.8	0				1	
1.5	0.8	1.7	6.8	0			9	
2	1.1	2.5	13.5	23.6	0		41	
2.1	1.2	3.3	20.3	47.2	21.0	0	93	
2.6	0.9	3.5	27.1	70.8	42.0	9.5	154	
3.1	0.8	2.8	28.4	94.5	63.0	19.1	209	
3.6	0.7	2.4	23.0	99.2	84.0	28.6	238	Peak flood
4.1	0.6	2.0	19.3	80.1	88.2	38.1	228	
4.6	0.5	1.8	16.6	67.2	71.2	40.0	197	
5.5	0	1.6	14.6	57.9	59.7	32.3	166	
6		0	13.0	50.8	51.4	27.1	142	
6.5			0	45.3	45.2	23.3	114	
7				0	40.2	20.5	61	
7.5					0	18.3	18	
8						0	0	

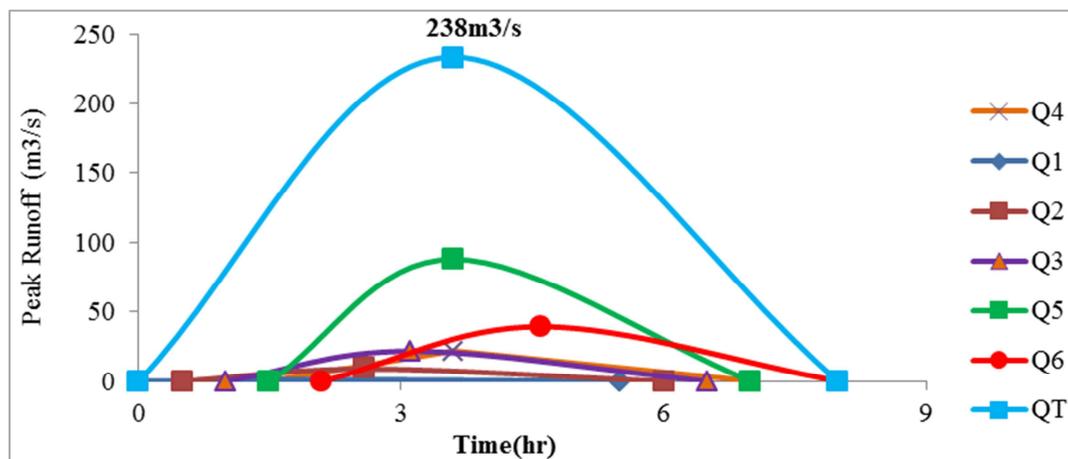


Figure 5. Composite hydrograph of Basaka sub-watershed once in 50 years return period.

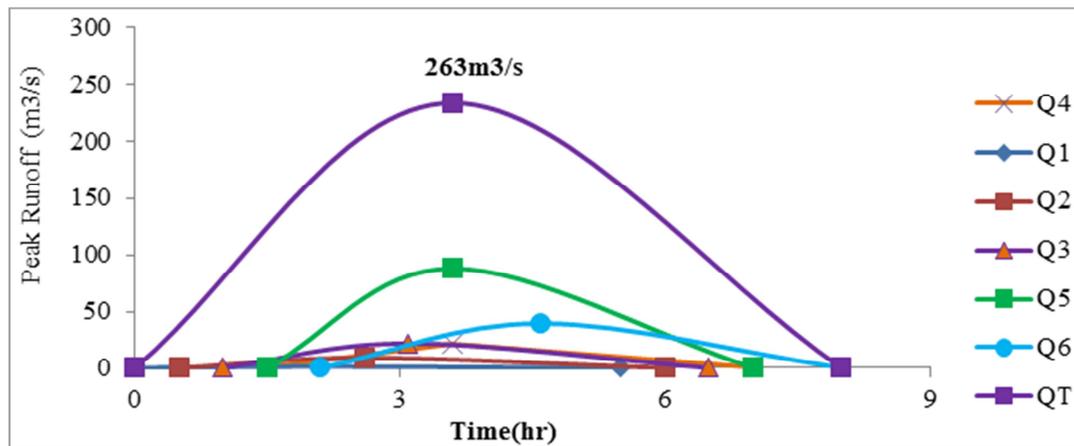


Figure 6. Composite hydrograph of Basaka sub-watershed once in 100 years return period.

4. Conclusion

This study was carried out to assess Hydrological Analysis and peak runoff determination. Hydrological analysis has been conducted based on 33 years of maximum daily rainfall data. The occurrence analysis has been carried out by using the Gumbel method. Because this is the most common distribution used to fit extreme rainfall events. Hence, this distribution has been selected as the best fit for this study. There is no gauging station on the Basaka River or nearby rivers of similar catchment characteristics. Thus, it is preferred to base the flood analysis on rainfall data, which are better both in quantity and quality of data. In general, estimating flood magnitude was done by the SCS method can be applied to the ungauged catchment. Since the catchment area of the Basaka River sub-watershed is 58 km², the SCS method is preferred. The SCS hydrograph method is selected for the analysis of the rainfall-runoff hydrograph and computation of the peak flood. The Peak runoff for the Basaka River sub-watershed corresponding to a return period of 50 & 100 years comes out as 238 & 263 m³/s respectively. Generally, the steps used during the estimation of peak flood once in a 50-year return period are also used to determine peak runoff once in a 100-year return period.

Data Availability

The data used to support the findings of the study are included within the article and are also available from the corresponding author upon request.

Acknowledgments

First of all, I would like to thank the Ethiopian Meteorological Institute (EMI) for providing the necessary data for the research without payment. Secondly, I would like to express my sincere gratitude to my special group of friends who also supported me through their friendship and who stood with me through contributions to his appreciable ideas. Last but not least, I would like to express my deepest gratitude to Wallaga University.

Conflict of Interest

The authors declare that they have no conflicts of interest.

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